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專利名稱: 大量焊接系統

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(美國)

申請專利範圍:

1. 一種利用焊料將電路板預側表面與底側表面所附裝之電氣與電子組件大量集體焊接之裝置，其特徵在於包含下述之組合：

大量焊接站(46)，可將一定量之熔融焊料澱積於該電路板底側表面與附裝於其上之任何組件上，以便將該組件於電氣上與機械上連接於該電路板底側；

焊料再流動站(110)，可將該電路板頂側表面加熱至足以使其上面之焊料胚及/或焊料膏再流動，以便將其上面之任何組件於電氣上與機械上連接於該電路板之頂側表面；以及

輸送設備(120)，用於將該電路板在該大量焊接站與該焊料再流動站之間依一定之時序串列輸送，該一定之時序被調整設定，以當通過該電路板之熱量傳送達到其最大值之時刻附近將該電路板帶入該再流動站。

2. 根據請求專利部份第 1. 項之裝置，其特徵在於，包括裝設於該大量焊接站

(46)與該焊料再流動站(110)

之間以當電路板在該焊接站之間輸送之際維持電路板溫度用之至少一個輻射加熱器(112)。

3.根據請求專利部份第 1.或 2.項之裝置

，其特徵在於，包括在該大量焊接站附近而且在該大量焊接站直後之過量焊料移除站(100)，該過量焊料移除站含有：至少一個氣體噴射嘴(

102)，在該電路板行進路徑之下方而且可在該焊料完全凝固之前將流體流導引至該電路板底側表面之新澱積的焊料與其上之組件上；壓力流體源，最好為壓力空氣源；以及，將該壓力流體源與該至少一個噴射嘴相連接之連接設備，該過量焊料移除站可在該熔融焊料凝固成為垂柱及/或跨接件之前將澱積於該電路板底側表面上之該熔融焊料之一部份重整或移除。

4.根據請求專利部份第 1.至 3.項任何一項之裝置，其特徵在於，該再流動站

含有：至少一個氣體噴射(114, 116)，在該電路板行進路徑之上方而且可將流體氣體流導引至該電路板頂側表面上；壓力流體源，最好為壓力空氣源，與將該壓力流體源與該至少一個流體噴射嘴相連接之連接設備；以及，加熱設備，用於將該流體加熱至足以將該電路板頂側表面之溫度提高而使其上之任何焊料胚、焊料膏再流動之溫度。

5.根據請求專利部份第 4.項之裝置，其特徵在於，包括至少兩個氣體噴射嘴(114,116)，實質上垂直向下而且沿該行進路徑排列。

6.根據請求專利部份第 4.項之裝置，其特徵在於，包括用於將該空氣加熱至 350° ~425℃ 範圍之溫度之加熱設

備。

7.根據請求專利部份第 1.至 6.項任何一項之裝置，其特徵在於，該大量焊接站含有由形成波浪之第一個與第二個焊料槽構成之整體總成(46)。

8.根據請求專利部份第 7.項之裝置，其特徵在於，該第一個焊料槽(60)含有一個槽與一個噴嘴，能夠產生具有較大垂直動量成份之窄小波浪，而該第二個焊料槽(62)含有一個槽與一個噴嘴，能夠產生實質上單向之焊料波浪，其流動方向反對於該電路板之輸送方向。

9.一種利用焊料將電路板上下兩面之電氣與電子組件大量集體焊接之方法，該方法之特徵包含下述步驟：

將熔融焊料澱積於該電路板底側表面及其上之組件上，並允許焊料凝固於其上，

保持該電路板以允許該電路板底側表面上之熱能通過電路板而上昇至該電路板頂側表面而且經由該電路板之傳熱作用而達到實質上最大溫度；

以及

繼之立即將電路板頂側表面加熱至足以使其上之任何焊料胚或焊料膏再流動之溫度。

10.根據請求專利部份第 9.項之方法，其特徵在於，該加熱至再流動係在將該熔融焊料塗施至該電路板底側表面之後大約 15 至 20 秒以內完成。

11.根據請求專利部份第 9.或 10.項之方法，其特徵在於，當該保持期間將該電路板維持於高溫或絕熱環境內之步驟

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## MASS SOLDERING SYSTEM

### Background of the Invention

This invention relates to systems for soldering electrical and electronic components onto substrate boards, and more particularly to an improved apparatus and method for mass soldering electrical and electronic components to the top and bottom surfaces of substrate circuit boards or the like in a single pass. The invention has particular application to soldering of surface mounted components such as chips or the like to both top and bottom surfaces of printed circuit boards and will be described in connection with such application. It will be understood, however, that the invention also may be used for soldering circuit boards having only conventional through-hole mounted components on the top surface alone, surface mounted components on the bottom surface alone or the combination of the two, and circuit boards having both conventional through-hole mounted components and surface mounted components on the top surface and surface mounted components on the bottom surface.

In response to recent demands for compact electronic appliances and instruments, there has been a tendency to use small, thin chip type electronic parts, i.e., surface mounted components and/or carriers therefor, for mounting on printed circuit boards in place of conventional, discrete type, leaded components. The advent of surface mounted component technology has afforded striking new levels of efficiency to the circuit board designer and, at the same time, has posed new challenges for the manufacturing engineer. Apart from the frequently noted advantages of component size and geometry, the circuit board designer has at his disposal the capability of populating both top and bottom surfaces of printed circuit boards with

components.

Various techniques have been proposed by the art for mass soldering surface mounted components to a single sided circuit board. One technique involves fixturing the components to the bottom side surface of the board, e.g., using an epoxy adhesive or the like, and then engaging the bottom surface of the board and fixtured components with molten solder by passing the board bottom surface and fixtured components in contact with a body of molten solder as, for example, through the crest of a standing solder wave. Such a process is described in U.S. Patent 4,465,219 to Kenshi Kondo.

It has also been proposed to solder surface mounted components to the top surface of a circuit board using a solder cream or paste, or a solder preform or the like. In such prior art technique, the surface mounted components are loaded in position on the top side surface of the board, together with suitable solder preforms or a solder cream or paste, and the circuit board and loaded components are heated to a temperature sufficient to reflow the solder. Heating to effect solder reflow can be accomplished by baking the circuit board and components in a radiant furnace or the like. Alternatively, the circuit board and components may be immersed in a vapor heated to a temperature above the melting point of the solder, in accordance with the so-called vapor phase soldering or condensation soldering process. Such a process is described in U.S. Patent Nos. 3,866,307 and 4,321,031, which are given as exemplary. Radiant heating reflow soldering and vapor (condensation) soldering have achieved a certain degree of commercial acceptance although each technique has certain drawbacks. For one, the techniques are somewhat slow, and both techniques have a tendency to overheat components which could cause damage to heat sensitive

components. Also radiant heating reflow soldering is susceptible to line-of-sight shadowing and thus may not be entirely satisfactory for high density applications. Furthermore, the fluid used to create the vapor for  
5 condensation soldering is quite expensive, and the thermal decomposition products of the fluid produced are dangerous to health.

While such prior art systems, in spite of the aforesaid and other disadvantages, are being used to  
10 solder surface mounted components to one surface of a circuit board, no system was heretofore available for mass soldering components populating both (opposed) surfaces of a printed circuit board in a single pass.

It is thus a primary object of the present invention  
15 to provide a mass soldering system, i.e., apparatus and process, which overcomes the aforesaid problems of the prior art.

Another object of the present invention is to provide an improved apparatus and process for mass  
20 soldering components to both (opposed) surfaces of a circuit board in a single pass.

Still other objects will appear obvious and in part will appear hereinafter.

The invention accordingly comprises the processes  
25 involving the several steps and relative order of one or more of such steps with respect to each other and the apparatus possessing the features, properties and relations of elements which are exemplified in the following detailed description and the scope of the  
30 application of which will be indicated in the claims.

In the following detailed description of the invention, the term "component" refers to so-called leadless components such as chip components as well as components having conventional metallic conductors or  
35 leads. The term "component lead" refers to that part of

the metal conductor of an electrical or electronic component that is joined to the printed circuit board pattern, i.e. the component leads, terminals, lugs, pins, et cetera. The term "land" as used herein refers to that part of the metallic pattern on the printed circuit board to which a component or component lead is joined by solder. The terms "top side surface" and "bottom side surface" as used herein with reference to the circuit board are meant simply to refer to the opposed broad surfaces of the circuit board; the terms "top" and "bottom" respectively denote spatial orientation of the circuit board only as it is being processed in the soldering apparatus in accordance with the present invention. The term "mass soldering" as used herein is intended to refer to any of the several soldering techniques known in the art in which (a) molten solder is applied to a circuit board from a body of molten solder, including by way of example, but not limitation: wave soldering, dip soldering, pot soldering, jet soldering, cascade soldering and drag soldering, or (b) a plurality of solder connections are made essentially simultaneously by reflow of pre-applied solder preforms or solder cream or paste on a circuit board.

The present invention provides a novel system, i.e. method and apparatus, by which components populating both (opposed) surfaces of a printed circuit board may be mechanically and electrically joined to the printed circuit board by mass soldering in a single pass. More particularly, in accordance with the process aspect of the present invention, a circuit board containing components populating both top and bottom surfaces of the board is first subjected to a first mass soldering operation in which the bottom side surface of the board and components thereon are passed in contact with a body



of molten solder as by passing through the crest of a standing solder wave. The first mass soldering operation also imparts substantial heat energy to the board which heat energy is conducted through to the top side surface of the board. Additional heat energy then is supplied to the top side surface of the board to reflow preapplied solder cream or paste or solder preforms on the board top side surface. The apparatus of the present invention comprises a fluxing station wherein flux may be applied to the bottom surface of the circuit board; a preheater station wherein the flux is activated and the board prepared for soldering; a first mass soldering station wherein the bottom side surface of the printed circuit board may be brought into contact with a pool of molten solder; and a second mass soldering station wherein preapplied solder cream or paste or solder preforms on the top side surface of the printed circuit board may be heated to reflow. In a preferred embodiment of the invention the first soldering station comprises a wave soldering assembly consisting of two wave-forming solder sumps including a first nozzle for forming a bidirectional wave and a second nozzle for forming a second substantially unidirectional wave, and the second mass soldering station comprises a convection heating assembly consisting of a pair of heated nozzles for directing heated fluid streams substantially vertically downwardly onto the top side surface of the board. In a particularly preferred embodiment of the invention the heated fluid comprises heated air. Completing the apparatus is means for transporting the circuit boards to be soldered in-line in timed sequence between the first mass soldering station and the second mass soldering (reflow) station.

For a fuller understanding of the object of the present invention, reference should be had to the following detailed description taken in connection with the accompanying drawings in which:

5        Fig. 1 is a flow diagram showing the various steps in the process of the present invention;

      Fig. 2 is a side elevational view, diagrammatically illustrating a mass soldering system according to the present invention;

10       Fig. 3 is an enlarged diagrammatic view of a preferred form of the first mass soldering station section of the apparatus in accordance with the present invention;

      Fig. 4 is an enlarged diagrammatic view of a preferred form of the second mass soldering (reflow) station section of the apparatus in accordance with the present invention; and

15       Fig. 5 is a graph illustrating measurements representing time/temperature profiles of the top side surface of circuit boards being processed in accordance with the teachings of the present invention.

      In the several drawings like numerals refer to like parts.

25       Referring to Figures 1 and 2, a printed circuit board 20 is loaded at an insertion station 22, with a plurality of electrical or electronic components 24, 26 at predetermined positions on the board. Board 20 comprises an insulated wiring board having one or more printed metallic conductors on the board bottom side surface 28 and one or more printed metallic conductors on the board top side surface 30. Components 24 are temporarily affixed in known manner in suitable locations on the board bottom side surface 28 by means of an adhesive such as a heat resistant epoxy adhesive or the like. Similarly, surface mounted components or

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the like 26 are temporarily affixed to the board top side surface 30 by means of solder paste or the like applied to the component leads and circuit lands. If desired, components 26 also may be affixed to the circuit board by means of an epoxy adhesive or the like.

The next step involves treating the bottom side surface of the board with a so-called flux at a fluxing station 40. The flux may be any flux well known in the art, and may include, for example a water-white rosin, an activated rosin flux or a water soluble flux. The flux may be applied at fluxing station 40 by any manner well known in the art for example by spraying, foaming, brushing or from a flux wave.

The board is then passed from fluxing station 40 to a preheating station 42 where the board is preheated to mobilize the flux, and the bulk of the flux solvent is driven off to form an active flux layer on the board and component leads. Preheating station 42 may comprise radiant or convection heaters or a combination of radiant and convection heaters as are well known in the art.

The fluxed preheated board is then passed to a first mass soldering station 46 which in a preferred embodiment of the invention comprises an integrated assembly of two wave soldering sumps and nozzles. Referring to Figs. 2 and 3, mass soldering station 46 comprises a container of conventional design, indicated generally at 50 for holding a supply of molten solder 52. Conventional heating means (not shown) may be secured to the bottom and/or side walls of container 50 or immersed in the solder to heat and maintain the supply of solder 52 in molten condition.

First and second sump and nozzle assemblies indicated generally at 60 and 62, respectively, are disposed interiorly of container 50. First sump and

nozzle assembly 60 typically comprises a bottom wall 64, a pair of inclined side walls 66, 68, and a pair of substantially vertically opposed end walls only one of which 70 is shown. The upper ends of the end walls 70 and side walls 66 and 68 are spaced from one another to form a narrow elongated rectangular nozzle or slot 72 which extends above the molten solder level in container 50 a suitable distance, e.g. one inch above the molten solder level.

10 Preferably the sump also includes a pair of adjustable sluice plates 76A, B, spaced from the sump side walls 66 and 68 for controlling the solder overflow from the nozzle 60, e.g. in accordance with the teachings of U.S. Patent 3,398,873 to Kenneth G. Boynton. A variable speed pump (not shown) communicating through an inlet orifice 78 in the lower end of sump and nozzle assembly 60 is provided for pumping solder in the sump where it rises and overflows the nozzle 72 as a narrow solder wave being a relatively large vertical component of momentum.

The second sump and nozzle assembly 62 comprises a sump and nozzle assembly made in accordance with the teachings of U.S. Patent 4,208,002 to Matthias F. Comerford, et al. The second sump and nozzle assembly 62 thus comprises upwardly diagonally extending front wall 80 and a rear wall 82, and pair of vertically extending side walls 86 (only one of which is shown) connecting the front and rear walls to define a nozzle chamber 88 in the form of an upwardly extending open-ended chamber of increasing plan area. A Z-shaped baffle screen 90 is positioned within the nozzle chamber 88 and distributes the molten solder pumped upwardly in the sump as a wide, smooth substantially unidirectional solder wave. A second variable speed pump (not shown) independently adjustable from the first variable speed

pump, communicates through an intake orifice 94 located in the lower end of sump and nozzle assembly 62 for pumping molten solder into the sump where it then rises and overflows the nozzle 88 as a substantially  
5 unidirectional, standing soldering wave, whose flow direction (arrow 96) is counter to the direction of the board and conveyor travel as indicated by arrow 98. Preferably, sump and nozzle assembly 62 is arranged for oil intermix operation in accordance with the teachings  
10 of U.S. Patent 3,058,441 to Walker et al.

Immediately following the first mass soldering station 46 is an excess solder removal station 100 which is optional but preferred. Excess solder removal station 100 follows first mass soldering station 42  
15 immediately in-line and is designed to remove and/or relocate solder on the board underside and any interconnections, component leads and/or component bodies carried thereon before the solder solidifies as shorts, icicles and/or bridges, i.e., in accordance with  
20 the teachings of U.S. Patent 4,410,126 to Harold T. O'Rourke. Solder removal station 100 comprises one or more heated fluid jets, fluid knives, slots, nozzles or the like indicated generally at 102 from which a heated fluid stream, preferably hot air, is directed onto the  
25 underside of the board. Inert gas may be used as the fluid, but preferably the fluid comprises heated air. The hot air blast also shapes the fillets of surface mounted components, and it relocates the molten solder on the board so as to assure good solder coverage over  
30 the entire board including recesses between adjacent chip components. Solder removal station 100 also permits the use of a horizontal conveyor which has certain advantages as will be described hereinafter. Hot air knife 102 should be oriented so as to direct the  
35 hot air blast in a direction opposite to the direction

of board travel. Generally, nozzle 102 is disposed at an angle of between about  $30^{\circ}$  and about  $80^{\circ}$  from the horizontal, and preferably is at an angle of between about  $58^{\circ}$  and about  $65^{\circ}$  from the horizontal. The  
5 exact angle may be varied depending on the angle of travel path of the board. In the case of a substantially horizontal conveyor, nozzle 102 preferably is at an angle of about  $60^{\circ}$  from the horizontal.

The air should be preheated to a temperature at  
10 least equal to the liquidus temperature of the solder, and preferably will be at a temperature of about 90 to  $200^{\circ}\text{C}$  (measured from the outlet of nozzle 102) higher than the liquidus temperature of the solder. For 63/37 solder alloy, the air should be heated to a temperature  
15 of about  $395^{\circ}\text{C}$  (measured at the outlet of nozzle 102).

As taught in U.S. Patent 4,410,126 to Harold T. O'Rourke, the fluid (hot air) stream impinging on the still molten solder contained on the underside of the circuit board, the interconnections and component leads  
20 and/or component bodies should have sufficient velocity to relocate excess solder on and/or blast excess solder from the underside of the board, inter-connections, leads and bodies so as to minimize the possibility of icicling or short formation upon solidification, but  
25 should not be so great as to disturb adequately wetted solder connections. Generally, in the case of air heated to a temperature of about  $395^{\circ}\text{C}$ , the air should have a fluid velocity (measured at the outlet of nozzle 102) of between about one and about two m/sec. The  
30 appropriate temperature/pressure parameters may be determined empirically. If desired a minor amount, e.g. up to about 20% by weight of liquid droplets, e.g. soldering oil and/or liquid flux also may be included in the fluid stream as by aspirating the liquid into the  
35 fluid stream as taught in O'Rourke U.S. Patent 4,410,126.

As will be appreciated, passing the circuit board 20 and components through the dual soldering waves and over the optional heated air knife imparts substantial heat energy into the bottom side surface of circuit board.

5 However, inasmuch as circuit boards per se are not good thermal conductors, the heat energy imparted to the board bottom side surface only slowly rises through the board to the top side surface. It has been observed that in the case of a two sided circuit board formed of

10 phenolic and having a board thickness of about 62 mil, there is a 15 to 20 second time lag between emergence of the board from the second solder wave and maximization of temperature on the board top side surface. Moreover, the temperature ultimately reached by the board top side

15 surface from heat inputted from the solder waves and the optional heated air knife is not sufficient by itself to produce fusing of the solder cream or paste and/or preforms on the board top side surface. The present invention makes maximum use of the heat inputted from the

20 wave soldering operation, and adds sufficient additional heat to raise the temperature of the top side surface of the board sufficiently high to reflow the solder cream or paste and/or preforms on the board top side surface. This can be accomplished at a top side solder reflow

25 station 110 as will be described in detail hereinafter.

As noted supra, there is a time lag between emergence of the board from the second solder wave and maximization of temperature on the board top side surface. In order to minimize heat energy loss from the

30 circuit board during this time lag, a post soldering holding station 111 preferably is located between mass wave soldering station 46 and reflow station 110. Post soldering holding station 111 preferably includes one or more heat reflectors 113 located under the travel path

35 of the boards, and one or more heaters 112 located over

the travel path of the boards. While post soldering heaters 112 may add some heat to the circuit boards being processed, the primary function of the post soldering heaters 112 is to maintain the temperature environment of the board as the heat from the bottom side surface of the board rises through the board to the top side surface. The post soldering heaters may comprise radiant or convection heaters or a combination of radiant and convection heaters as are well known in the art. Preferably, post soldering heaters 112 comprise one or a plurality of parabolic infrared heaters mounted over the top side surface of the board.

Following immediately post soldering heaters 112 in-line is reflow station 110. Reflow station 110 may comprise a radiant furnace, but preferably comprises one or more heated knives, fluid jets, slots, nozzles or the like indicated at 114 and 116, from which a low pressure heated fluid stream is directed to the top side surface of the board. Fluid knives 114 and 116 are similar in construction to fluid nozzle 102 and are arranged to impinge a stream of heated fluid, preferably heated air, onto the top side surface of the board. A single air knife can be used under certain circumstances; however, it has been found that the temperature spike achieved through the use of a single air knife typically does not raise the top side surface temperature of the board sufficiently high to effect reflow. On the other hand, it has been found that the combination of two closely spaced hot air knives, e.g. 4.5 inches apart directly over the circuit board, e.g. within about 1/8-1/4 inches above the circuit board, unexpectedly spike the top side surface of the board to a temperature sufficiently high to effect reflow. This is shown in Fig. 5, which illustrates time/temperature profiles of the top side



surface of a circuit board processed in accordance with the present invention.

Air knives 114 and 116 should be adapted to preheat the air to a temperature of in the range of 350-425°C so as to provide the desired temperature spike. Unlike the debridging nozzle 102 provided adjacent the wave soldering station 46 of the apparatus, the air velocity through nozzles 114 and 116 should be adjusted to be quite low and typically may be 1/10th to 1/15th of the velocity of the air emerging from nozzle 102. Air flow rate, air temperature, pressure and the time elapsed between circuit board emerging from the wave soldering station and beginning of contact by the heated air stream on the board top side surface may vary widely depending on board thickness, ambient temperature, melting point of the solder preforms or solder cream or paste, specific heat of gas or air, heat transfer co-efficient of gas to the board, board size and shape, component density, amount of solder preforms or solder cream or paste deposited, conveyor speed and distance between the soldering station 62 and reflow station 110. As noted supra, it has been determined empirically that a 15 to 20 second lag exists between emergence of the circuit board from the solder wave to maximization of temperature on the top side surface of the printed circuit board. Thus, the conveyor speed and distance between solder wave station 62 and reflow station 110 should be selected as to take advantage of the maximization of top side temperature.

The solder cream or paste may comprise any commercially available solder cream or paste. Preferably the solder cream or paste comprises solder powder on the order of 350 mesh suspended in a fluxing material and a vehicle. Preferably but not necessarily the solder cream or paste will be of the same chemical

composition as the solder utilized in the wave soldering station so that constituents of the solder on both top and bottom surfaces of the solder board will be identical. Various solder creams and pastes are  
5 available commercially and may be utilized in accordance with the present invention.

Completing the apparatus is a conveyor system 120. The latter is of conventional construction and typically comprises a pair of spaced conveyor rails 122 and 124  
10 and suitable drive means (not shown). Preferably conveyor system 110 operates substantially in the horizontal plane so that the boards being processed are carried by conveyor 120 along a substantially horizontal travel path. The provision of the air knife 102  
15 immediately following the second solder sump and nozzle 62 assures bridge-free soldering even in the horizontal mode. Operating in the horizontal mode minimizes possible problems of component shifting on the board top side surface. Employing a horizontal transport system  
20 also simplifies loading and unloading transitions.

A particular feature and advantage of the present invention is the ability to mass solder both sides of a circuit board in a single pass through the soldering system. This results in substantial manufacturing  
25 economies, and in addition limits temperature cycling of the circuit board assembly to a single cycle.

Various changes may be made in the foregoing invention without departing from the inventive features described herein. For example, three or more heated air  
30 knives may be employed in the reflow (fusing) station 110 if additional thermal "kick" is required, e.g. as in the case of particularly high density boards. Also, reflow (fusing) station 110 may comprise radiant heaters or a combination of radiant and convection heaters.  
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Also, if desired, a final cooling nozzle (not shown) may be provided following reflow station 110.

Still other changes may be made in accordance with the present invention without departing from the spirit  
5 and scope thereof. Accordingly, it is intended that all matter contained in the above description or shown in the accompanying drawings shall be interpreted in an illustrating and not in a limiting sense.

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CLAIMS

1. Apparatus for mass joining with solder electrical and electronic components affixed on a circuit board and populating both the top side surface of the board and the bottom side surface of the board, and characterized comprising in combination:

a mass soldering station (46) adapted to deposit a quantity of molten solder onto the bottom side surface of said board and any components affixed thereto whereby to electrically and mechanically join said components to the bottom side of said board;

a solder reflow station (110) adapted to heat the top side surface of said board sufficient to reflow solder preforms and/or solder paste or cream thereon whereby to electrically and mechanically join any components thereon to the top side surface of said board; and

means (120) for transporting said circuit board in line between said mass soldering station and said solder reflow station in timed sequence, said timed sequence being adjusted to bring said board into said reflow station at or near the time at which heat transfer through said board has reached its maximum amount.

2. Apparatus according to claim 1, and characterized by including heating means (112), preferably at least one radiant heater located between said mass soldering station (46) and said solder reflow station (110) for maintaining the temperature of the board as it is transported between said soldering stations.

3. Apparatus according to claim 1 or 2, and characterized by including an excess solder removal station (100) adjacent said mass soldering station and following immediately thereafter, said excess solder removal station comprising at least one gas jet (102)

disposed below the travel path of said board and adapted to direct a fluid stream onto the freshly deposited solder on said bottom side surface of said board and components thereon before said solder fully solidifies thereon, a source of pressurized fluid, preferably pressurized air, and means connecting said source and said at least one jet; said excess solder removal station being adapted to relocate or remove a portion of said molten solder deposited on said bottom side surface of said board and said components before said molten solder solidifies thereon as icicles and/or bridges.

4. Apparatus according to any of claims 1 to 3, characterized in that said reflow station comprises at least one gas jet (114,116) disposed above the travel path of said board and adapted to direct a fluid gas stream onto said board top side surface; a source of pressurized fluid, preferably pressurized air, and means connecting said source and said at least one fluid jet; and means for heating said fluid to a temperature sufficient to raise the temperature of said board top side surface to reflow any solder preforms, solder cream or solder paste thereon.

5. Apparatus according to claim 4, characterized by including at least two gas jets (114,116) substantially vertically downwardly directed, in line along said travel path.

6. Apparatus according to claim 4, characterized by including means for heating said air to a temperature in the range of 350 to 425°C.

7. Apparatus according to any of claims 1 to 6, characterized in that said mass soldering station comprises an integrated assembly (46) consisting of first and second wave forming solder sumps.

8. Apparatus according to claim 7, characterized in that said first solder sump (60) comprises a sump and

nozzle capable of producing a narrow wave having a relatively large vertical component of momentum, and said second solder sump (62) comprises a sump and nozzle capable of creating a substantially unidirectional  
5 solder wave whose flow is in a direction opposite to the direction of transport of said circuit board.

9. A method for mass joining with solder electrical and electronic components populating both sides of the circuit board, said method characterized by comprising  
10 the steps of:

depositing a quantity of molten solder onto the bottom side surface of said board and components thereon and permitting the solder to solidify thereon;

holding said board whereby to permit the heat energy  
15 on the bottom side surface of said board to rise through to the top side surface of said board and reach substantially maximum temperature due to heat transfer through said board; and

immediately thereafter heating the board top side  
20 surface to a temperature sufficient to reflow any solder preforms, solder creams or paste thereon.

10. A method according to claim 9, characterized in that said heating to reflow follows within about 15 to 20 seconds following application of said molten solder  
25 onto the bottom side surface of said board.

11. A method according to claim 9 or 10, characterized by including the step of maintaining said circuit board in a heated or insulated environment during said holding in order to minimize loss of heat  
30 energy from said board.

ABSTRACT

An improved apparatus and method for mass soldering electrical and electronic components populating both the top and bottom surfaces of substrate circuit boards or the like in a single pass is described.

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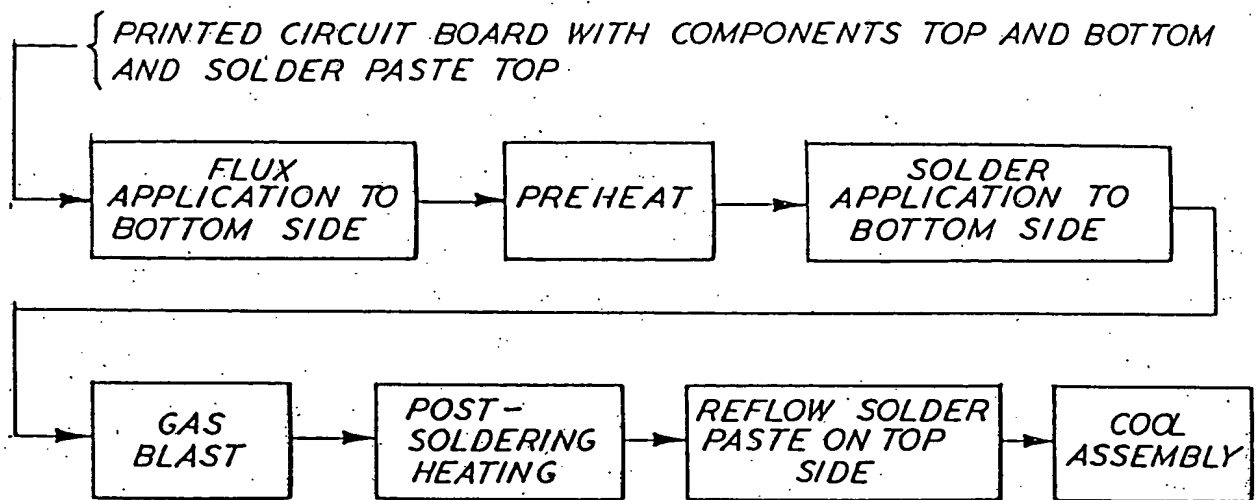


FIG. 1

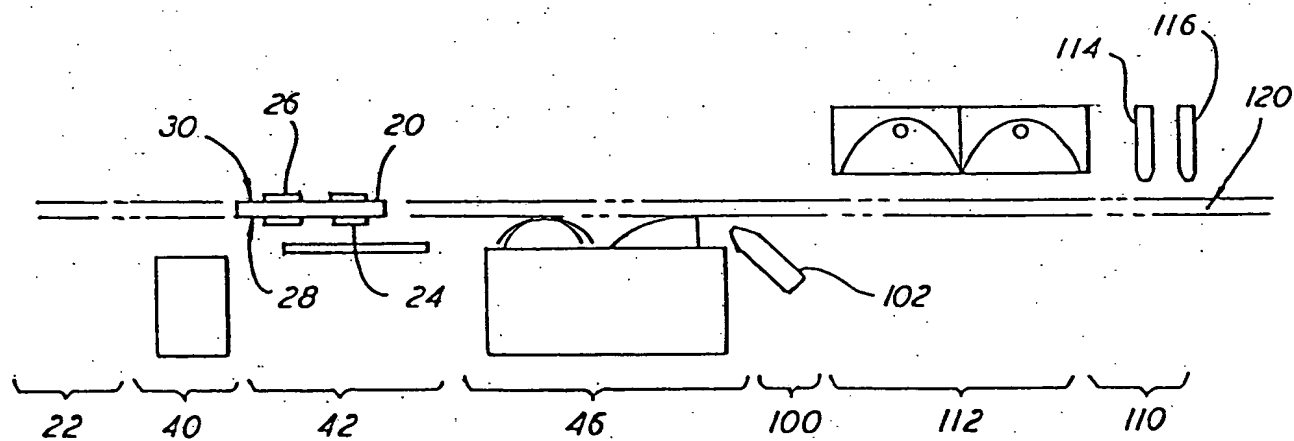


FIG. 2



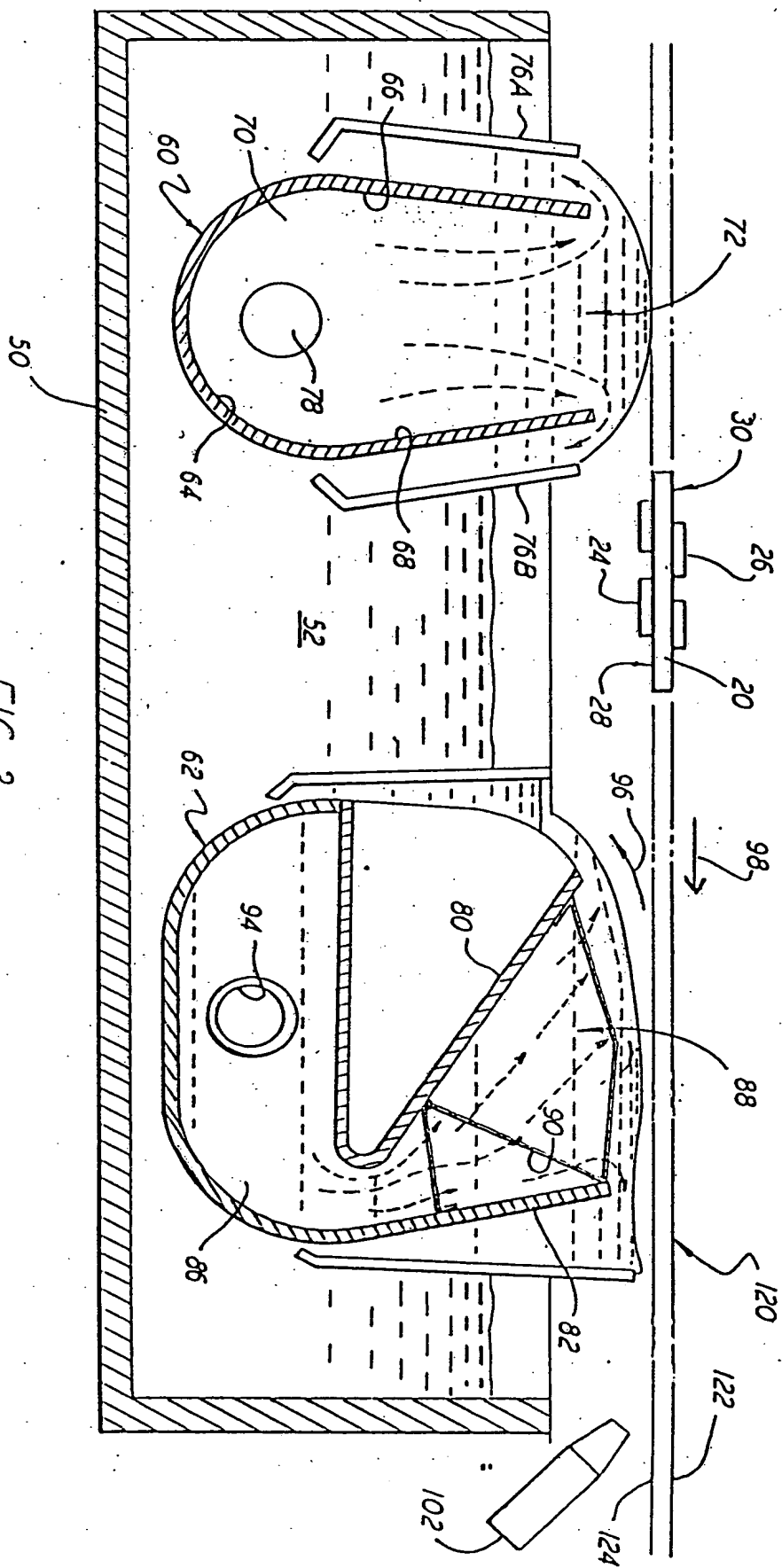
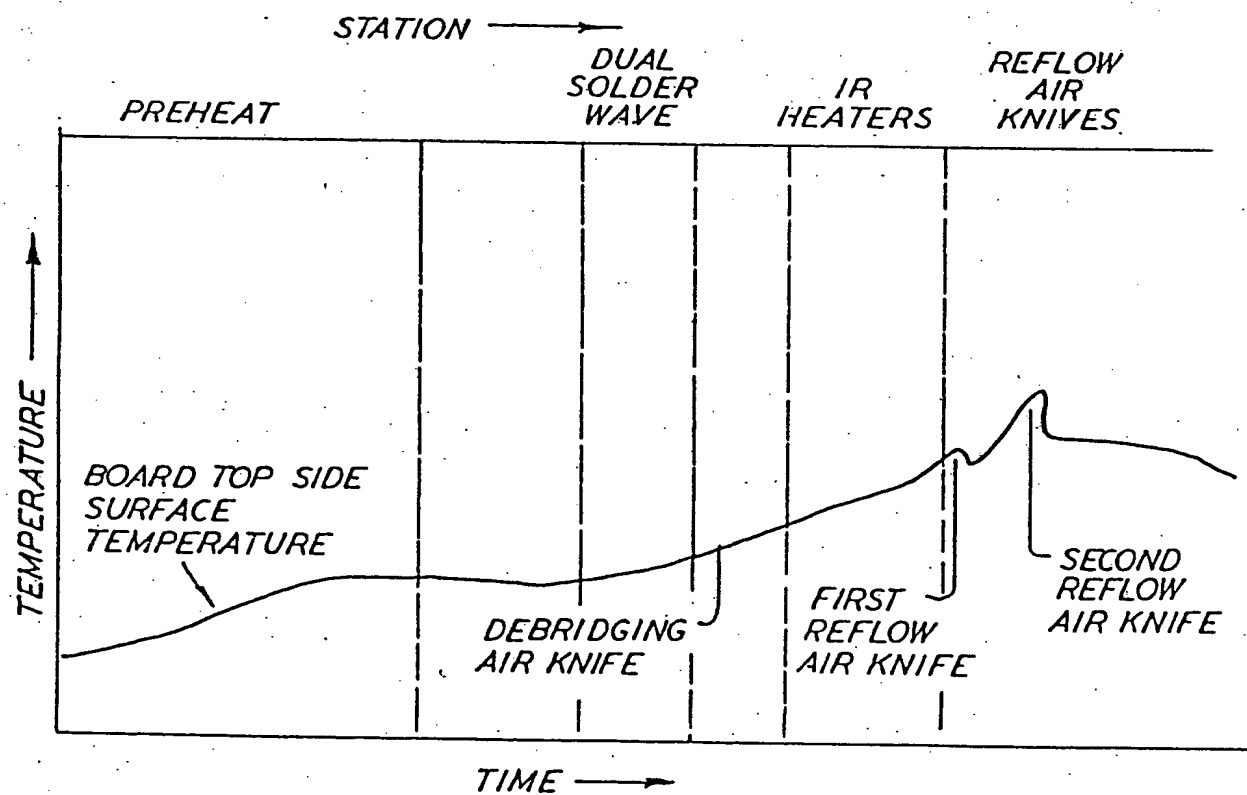
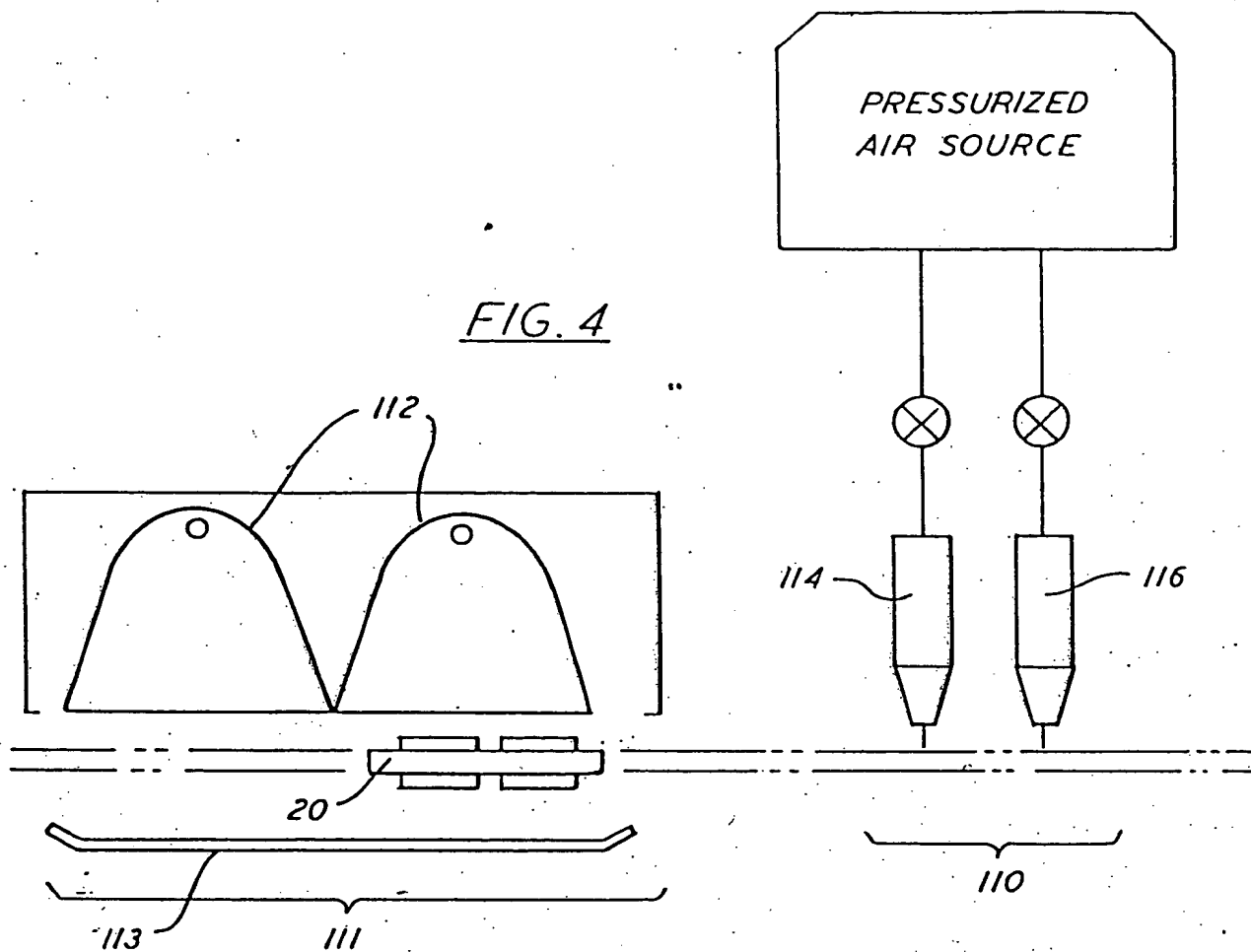


FIG. 3



**FIG. 5**